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**RESEARCH REPORT**  
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# Modelling of Density Limit Phenomena in Toroidal Helical Plasmas

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## Abstract

The physics of density limit phenomena in toroidal helical plasmas based on an analytic point model of toroidal plasmas is discussed. The combined mechanism of the transport and radiation loss of energy is analyzed, and the achievable density is derived. A scaling law of the density limit is discussed. The dependence of the critical density on the heating power, magnetic field, plasma size and safety factor in the case of L-mode energy confinement is explained. The dynamic evolution of the plasma energy and radiation loss is discussed. Assuming a simple model of density evolution, of a sudden loss of density if the temperature becomes lower than critical value, then a limit cycle oscillation is shown to occur. A condition that divides the limit cycle oscillation and the complete radiation collapse is discussed. This model seems to explain the density limit oscillation that has been observed on the W7-AS stellarator.

**keywords:** density limit, radiation loss, anomalous transport, L-mode scaling law, helical systems

## 1. Introduction

Recently, much attention has been paid to the density limit phenomena in toroidal helical plasmas [1-8]. The physics phenomenon, which occurs in the vicinity of the operational density limit, has various aspects of importance. Firstly, this process is considered to dictate the achievable plasma performance. The lack of toroidal symmetry could cause the enhancement of the energy loss in the long mean free path regime, and the anomalous transport also tends to increase (in the absence of the transition to an improved

confinement state) if the plasma temperature increases. Therefore the optimum fusion triplet, which is the product of density, ion temperature and confinement time, is expected in the high density regime. The density limit could impose an upper bound on the fusion triplet value. Secondly, in the W7-AS stellarator the H-mode, the most typical example of the improved confinement modes, occurs when the density becomes higher than the critical density for transition. Empirically, this critical density for the H-mode transition is known to become larger as the heating

power increases [9]. The knowledge of the operational density limit is necessary to establish the perspective for the realization of the H-mode with high heating power. Thirdly, plasmas in toroidal helical devices are operated mainly in a condition which are free from current-driven global MHD instabilities. Owing to this fact, precise experimental studies could be performed in toroidal helical plasmas even in the final phase of the radiation collapse. An attractive research area has been identified.

One important mechanism associated with the density limit phenomena is considered to be the radiation loss of line emission from impurity ions. The radiation loss can have a temperature dependence such that the loss increases if the temperature decreases [10]. Owing to this dependence, the radiation loss could cause the radiation collapse of plasma discharge in a similar fashion to detachment or MARFE formation [11]. A large scale deformation of the temperature profile often causes current disruption or strong degradation of confinement in tokamaks. This limit has been called the density limit in tokamaks [12]. The dynamics of radiation collapse also depends on the impurity species. When a heavy impurity like tungsten plays a dominant role, plasma with strongly hollow electron temperature profile is formed [13].

In toroidal helical devices the current disruption might not take place but a strong degradation of confinement occurs if radiation collapse happens. The transport of impurities in helical plasmas has been studied intensively [14, 15]. The limit of density due to radiation collapse has been studied and the dependence of

the critical density on the plasma heating power was derived [1]. An empirical scaling law for the density limit in helical devices has been presented and a dependency on the magnetic field has become clear [2, 8]. In addition, a periodic oscillation of the plasma energy in the vicinity of the density limit on LHD, CHS and W7-AS devices [5-8, 16] has been found recently. Such dynamics attract special interest because it is a characteristic example of self-sustained oscillation in confined plasmas.

In this article, we discuss the physics of the density limit phenomena based on an analytic model of toroidal helical plasmas. The combination of the transport loss of energy and radiation loss is analyzed and the scaling law for the density limit is derived. The parameter dependence of the critical density is explained. In the case of L-mode confinement, an approximate relation like  $n_c \sim P^{1/2} B^{1/2} V^{-1/3} q^{-1/4}$  is derived ( $P$  : heating power,  $B$  : magnetic field,  $V$  : plasma volume,  $q$  : safety factor). Then, the dynamical evolution of the plasma energy and radiation loss is discussed. By a method of reduction of variables, a simple model equation of the self-generated oscillation near the density limit is presented. A mechanism of density clump (i.e., rapid decay of density) at low plasma temperature is presented. A condition for the oscillation to occur when the density exceeds the density limit is derived.

## 2. Model of Density Limit

### 2.1 Point model

We start from the simple energy balance equation

$$\frac{d}{dt}W = -\frac{1}{\tau_E}W - P_{rad} + P \quad (1)$$

where  $W$  is the plasma energy,  $P_{rad}$  is the radiation loss,  $P$  is the heating power, and  $W/\tau_E$  are the other loss processes. We here consider that  $\tau_E$  is the energy confinement time governed by the transport processes. In the point model, the radiation loss is expressed as

$$P_{rad} = n_e n_i \langle L_Z(T) \rangle V \quad (2)$$

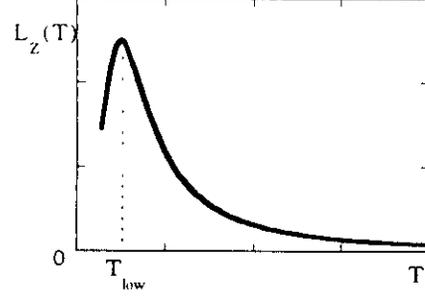
where  $n_e$  is the averaged electron energy,  $n_i$  is the averaged impurity ion density,  $T$  is the averaged electron temperature and  $V$  is the plasma volume. The radiation rate coefficient  $L_Z$  is usually defined as a local value, being a function of the local temperature. In this article, for the transparency of the analysis, we use a volume average value  $\langle L_Z(T) \rangle$ . This means that the influence of the profiles of temperature or density is included in the coefficient.

## 2.2 Stationary Solution

The stationary state is given by the relation

$$P = \frac{1}{\tau_E}W + P_{rad} \quad (3)$$

Model forms for the radiation loss and transport loss are introduced. The radiation rate coefficient has a dependence on temperature shown schematically in Fig. 1. Above a certain energy, which corresponds to the spectrum edge of impurity ions, it is a decreasing function of the temperature (until :



**Fig.1** Conceptual drawing of the radiation rate coefficient

next edge is reached). We therefore choose a simple power law form for the analytical study

$$\langle L_Z(T) \rangle = \xi T^{-\gamma} \quad (4)$$

in the range ( $T > T_{low}$ ). For simplicity, we assume that the lower limiting temperature,  $T_{low}$ , is much lower than the temperature which is realized by the balance of the input power and transport loss. The coefficient represents the species of ions and reflects the influence of profiles. By introducing this form of radiation rate coefficient, the radiation loss is expressed as :

$$P_{rad} = n^2 \left( \frac{n_i}{n} \right) \xi T^{-\gamma} V \quad (5)$$

In the following,  $n$  denotes the averaged electron density. The confinement time is also expressed in a similar way where the profile effect is included in  $\tau_{E0}$  as:

$$\tau_E = \tau_{E0} n^\beta T^{-\alpha} \quad (6)$$

The dependence of the density and temperature is explicitly separated, in order to illustrate the

dependence of the total loss on the density and temperature. The transport loss of energy is expressed as ( $W = 3nTV$ , assuming that  $T_e = T_i$ )

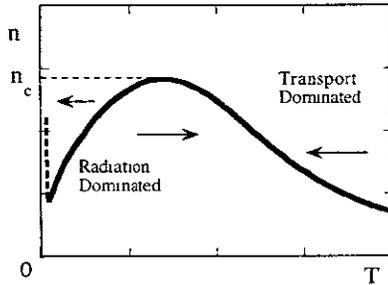
$$\frac{1}{\tau_E} W = \frac{3V}{\tau_{E0}} n^{1-\beta} T^{1+\alpha} \quad (7)$$

From Eqs.(5) and (7), the equation for the stationary state, Eq(3), is written as

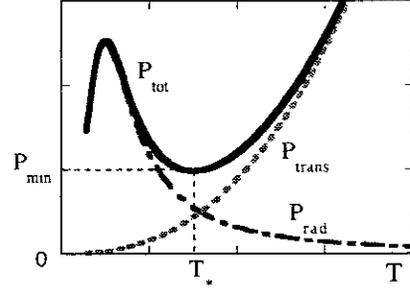
$$P = \frac{3V}{\tau_{E0}} n^{1-\beta} T^{1+\alpha} + V \left( \frac{n_i}{n} \right) \xi n^2 T^{-\gamma} \quad (8)$$

Equation (8) describes the relation between the plasma temperature and density under the given heating power  $P$ . Figure 2 illustrates the relation between  $T$  and  $n$ .

Equation (8) describes the accessible region of the density for the given heating power. The accessible density region is calculated from the total energy loss rate. The dependence of the total loss (i.e., the right hand side of Eq.(8),  $P_{tot} = P_{trans} + P_{rad}$ ) on the temperature is studied. The loss  $P_{tot}$  has an asymptotic form of  $T^{-\gamma}$



**Fig.2** Energy balance curve which satisfies Eq.(8) for a given power. There is an upper bound of density, above which the stationary solution does not exist. The curve in the region  $T < T_{low}$  is plotted by dotted line. Arrows indicates the direction of temperature evolution when the stationary condition is not satisfied.



**Fig.3** Loss power is shown as a function of temperature for the fixed density. Total loss has a minimum at  $T = T_*$ .

in the low temperature limit and  $T^{1+\alpha}$  in the high temperature limit. The right hand side of Eq.(8) increases both in the low and high temperature limits as is shown in Fig.3. It has the minimum value at the temperature  $T_*$ ,

$$P \geq P_{min} \quad (9)$$

$$P_{min} = C V \left( \frac{n_i}{n} \right)^{1/(1+\mu)} \xi^{1/(1+\mu)} \tau_{E0}^{-\mu/(1+\mu)} n^{(2+\mu-\beta\mu)/(1+\mu)} \quad (10)$$

where the abbreviation is made as

$$\mu = \frac{\gamma}{1+\alpha} \quad (11)$$

and the numerical coefficient  $C$  is given by  $C = (1+\mu) (\mu/3)^{-\mu/(1+\mu)}$ . The temperature  $T_*$  is given by:

$$T_* = \left\{ \frac{\mu}{3} \left( \frac{n_i}{n} \right) \xi \tau_{E0} n^{1+\beta} \right\}^{1/(1+\alpha+\gamma)} \quad (12)$$

At the condition of minimum loss, the relation

$$P_{rad} = \frac{1}{\mu} P_{trans} \quad (13)$$

holds.

### 2.3 Density Limit

Equation (10) describes the minimum and necessary heating power in order to realize the stationary solution in the presence of the radiation loss and the transport loss. The minimum value  $P_{\min}(n)$  is a function of the density. The condition,  $P \geq P_{\min}(n)$ , can be rewritten as

$$n \leq n_c \quad (14)$$

where the upper bound of the density is explicitly given as

$$n_c = C' V^{-(1+\mu)(2+\mu-\beta\mu)} \left(\frac{n_I}{n}\right)^{-1/(2+\mu-\beta\mu)} \times \xi^{-1/(2+\mu-\beta\mu)} \tau_{E0}^{\mu/(2+\mu-\beta\mu)} P^{(1+\mu)/(2+\mu-\beta\mu)} \quad (15)$$

In this expression, the numerical coefficient  $C'$  is given as  $C' = C^{-(1+\mu)(2+\mu-\beta\mu)}$ .

Equation (15) shows that various quantities dictate the upper bound of the density. We here introduce the separation of the critical density into two factors as

$$n_c = f_{cl} \cdot f_{cT} \quad (16)$$

where

$$f_{cl} = C' \left(\frac{n_I}{n}\right)^{-1/(2+\mu-\beta\mu)} \xi^{-1/(2+\mu-\beta\mu)} \quad (17)$$

and

$$f_{cT} = V^{-(1+\mu)(2+\mu-\beta\mu)} \tau_{E0}^{\mu/(2+\mu-\beta\mu)} P^{(1+\mu)/(2+\mu-\beta\mu)} \quad (18)$$

The factor  $f_{cl}$  comes from the specification concerning on the impurity ions (relative abundance, species or profile, etc.), and  $f_{cT}$  represents the impact of energy transport.

The critical density in Eq.(15) is defined such that the stationary equilibrium disappears above this critical density for other fixed parameters. The gradual degradation of energy confinement could occur when the density comes closer to the critical density. At this critical density,  $n = n_c$ , Eq.(13) holds, so that the transport loss is reduced from the total input power as  $P_{trans} = \mu P / (1 + \mu)$ . The total plasma energy,  $W = \tau_E P_{trans}$ , satisfies the relation

$$\frac{W}{P} = \frac{\mu}{1 + \mu} \tau_E \quad (19)$$

This shows the reduction of global energy confinement, that is the left hand side of Eq.(19), at the critical density.

### 2.4 Parameter dependence of critical density

By specifying the property of the transport loss, the dependence of the critical density on the plasma parameters is discussed.

The energy confinement time has dependencies on the magnetic field and plasma size, in addition to those on density and temperature. We use a form

$$\tau_E \propto B^{\alpha} L^{\alpha_3} q^{-\alpha_4} n^{\beta} T^{-\alpha} \quad (20)$$

where  $B$  is the magnetic field,  $q$  is a safety factor (inverse of the rotational transform) and  $L$  is the system size,

$$V = L^3 . \quad (21)$$

The dependence

$$\tau_{E0} \propto B^{a_2} L^{a_3} q^{-a_4} \quad (22)$$

is substituted in Eq.(18), and the following relation is obtained as

$$f_{cl} \propto P^{c_1} B^{c_2} L^{c_3} q^{-c_4} \quad (23)$$

where indices are given as

$$c_1 = \frac{1 + \alpha + \gamma}{2 + 2\alpha + (1 - \beta)\gamma} \quad (24-1)$$

$$c_2 = \frac{a_2 \gamma}{2 + 2\alpha + (1 - \beta)\gamma} \quad (24-2)$$

$$c_3 = \frac{3 + 3\alpha + (3 - a_3)\gamma}{2 + 2\alpha + (1 - \beta)\gamma} \quad (24-3)$$

and

$$c_4 = \frac{a_4 \gamma}{2 + 2\alpha + (1 - \beta)\gamma} \quad (24-4)$$

If the properties of impurity radiation are not altered and  $f_{cl}$  is considered to be constant, the parameter dependence of the critical density is derived as

$$n_c \propto P^{c_1} B^{c_2} L^{c_3} q^{-c_4} . \quad (25)$$

## 2.5 Case study for transport models

### 2.5.1 Empirical scaling for confinement time

Studies to correlate the confinement time with the input heating power have been made. Coefficients  $(\alpha, \beta, a_2, a_3, a_4)$  are fitted

from the empirical scaling law. The empirical dependence on the heating power is interpreted as the dependence on temperature.

In the limit where the transport process dominates the energy loss,  $W/\tau_E \gg P_{rad}$ , the energy balance equation is rewritten as  $3nTV = \tau_E P$ . Elimination of  $T$  from this relation by use of Eq.(4),  $\tau_E = \tau_{E0} n^\beta T^{-\alpha}$ , provides the energy confinement time as a function of heating power as

$$\tau_E = \tau_{E0}^{1/(1+\alpha)} L^{3\alpha/(1+\alpha)} n^{(\alpha+\beta)/(1+\alpha)} P^{-\alpha/(1+\alpha)} \quad (26)$$

Substituting Eq.(22) into  $\tau_{E0}$  of Eq.(26), the dependencies of energy confinement time can be derived:

$$\tau_E \propto n^{(\alpha+\beta)/(1+\alpha)} P^{-\alpha/(1+\alpha)} B^{a_2/(1+\alpha)} \times L^{(3\alpha+a_3)/(1+\alpha)} q^{-a_4/(1+\alpha)} . \quad (27)$$

The international stellarator scaling law (ISSL-95) [17] is used as a reference empirical formula :

$$\tau_E^{ISSL} \propto n^{0.51} P^{-0.59} B^{0.83} L^{2.86} q^{-0.4} . \quad (28)$$

Comparing Eqs.(27) and (28), the empirical scaling law (28) is interpreted as the confinement time with indices

$$\alpha \simeq 1.44 , \quad (29-1)$$

$$\beta \simeq -0.2 , \quad (29-2)$$

$$a_2 \simeq 2.03 , \quad (29-3)$$

$$a_3 = 2.66, \quad (29-4)$$

and

$$a_4 = 0.976 \quad (29-5)$$

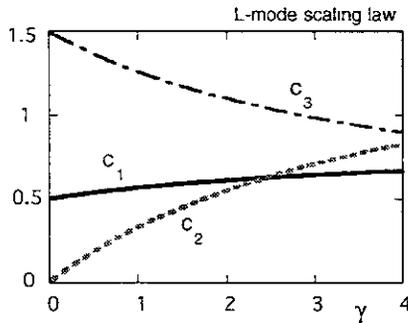
The values of these coefficients are substituted into the power indices for the critical density in Eqs.(24-1)-(24-4). The power indices  $(c_1, c_2, c_3)$  are shown as a function of  $\gamma$  in Fig.4. One sees that, in a wide range of the index  $\gamma$ , the power index  $c_1$  is approximately constant as

$$c_1 \sim \frac{1}{2}. \quad (30)$$

On the other hand, the indices to the magnetic field and to the system size depend on the value of  $\gamma$ . In the limit of  $\gamma = 0$ , indices are given as

$$(c_1, c_2, c_3, c_4) = (0.5, 0, 1.5, 0), \quad (31)$$

i.e.,  $n_c \propto \sqrt{PIV}$ , which corresponds to the



**Fig.4** Power index as a function of the gradient of radiation coefficient  $\gamma = -\partial \ln(L_Z) / \partial \ln(T)$ . Empirical scaling law, ISSL-95, is used for the model of energy transport.

simple estimate in which power dependence of  $L_Z$  was neglected [1]. In a more realistic regime,

$$\gamma - 2 \quad (32)$$

the indices are, very roughly speaking, given in the range of

$$(c_1, c_2, c_3, c_4) \sim \left(\frac{1}{2}, \frac{1}{2}, 1, \frac{1}{4}\right) \quad (33)$$

### 2.5.2 Deductive model of transport

Analysis is also performed for other transport models in which the transport coefficient is obtained by a deductive theory. We chose an example for the case of current-diffusive interchange mode turbulence [18]. This model has been shown to have considerable success in explaining the L-mode confinement. (The theory has also been extended to explain the H-mode, by introducing the effect of the radial electric field.) The formula of confinement time was deduced as

$$\tau_E \propto B^2 L^3 q^{-1} n^0 T^{-1.5}. \quad (34)$$

The indices  $(\alpha, \beta, a_2, a_3, a_4)$  are given as

$$(\alpha, \beta, a_2, a_3, a_4) = (1.5, 0, 2, 3, 1) \quad (35)$$

The indices for the density limit are then expressed as

$$c_1 = \frac{2.5 + \gamma}{5 + \gamma}, \quad (36-1)$$

$$c_2 = \frac{2\gamma}{5+\gamma}, \quad (36-2)$$

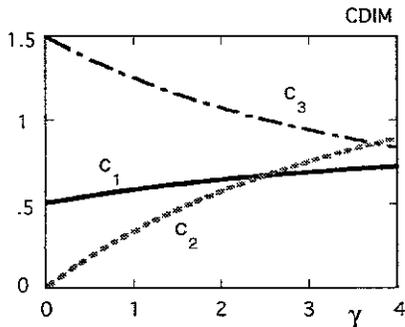
$$c_3 = \frac{7.5}{5+\gamma}, \quad (36-3)$$

$$c_4 = \frac{\gamma}{5+\gamma} \quad (36-4)$$

Figure 5 illustrates the dependence of coefficients on the parameter  $\gamma$ . Similar results are obtained in comparison with the case of the empirical form of transport loss.

## 2.6 Dependence of density limit

By considering the parameter dependence of the energy confinement time, the dependence of the critical density is deduced. A similar conclusion for the density limit is obtained when one employs either an empirical form of the energy confinement or a theoretical form of turbulent transport that is based on the current-diffusive interchange mode turbulence. This analysis shows that the relation  $c_1 \sim 0.5$  holds independent of the shape of the radiation curve  $\gamma = -d \ln(L_Z) / d \ln(T)$ , so long as the impurity ratio  $n_i/n_e$  remains unaltered. The



**Fig.5** Power index as a function of the gradient of radiation coefficient  $\gamma = -d \ln(L_Z) / d \ln(T)$ . Transport model is based on current-diffusive interchange mode.

dependence of the transport loss on the magnetic field introduces the influence of the magnetic field on the critical density. The dependence of the confinement time on the plasma size affects additionally the dependence of critical density on the system size. The scaling dependence of the density limit is also influenced by the coefficient  $\gamma$ . The approximate estimation Eq.(33),  $(c_1, c_2, c_3, c_4) \sim (\frac{1}{2}, \frac{1}{2}, 1, \frac{1}{4})$ , corresponds to an approximate form

$$n_c \sim P^{1/2} B^{1/2} V^{-1/3} q^{-1/4}. \quad (37)$$

This result is compared to the experimental observation [2, 8]

$$n_c \propto \sqrt{PB/V}$$

The dependence on the heating power and magnetic field is close to the observation; Dependence on the plasma size becomes weaker than  $n_c \propto V^{-1/2}$ .

## 3. Dynamics at the Density Limit

### 3.1 Dynamical models

On the curve of Fig.2, the stationary solution is possible. When only the temperature is considered to evolve and other parameters are fixed, the direction of arrow in Fig.2 indicates the evolution of temperature. In the region where the transport dominates, (i.e., the right part of the curve), the stationary solution is stable. However, in the region where the radiation loss dominates, the stationary solution is unstable. A small deviation from the stationary curve causes further deviation of temperature from the curve.

The dynamical evolution is discussed in this chapter. When the density becomes higher than  $n_c$ , the stationary solution is lost, and the temperature starts to change. The other parameters might change as well. New type of dynamics could occur by the combination of the variation of other parameters.

The radiation loss is dependent on the plasma temperature, electron density and the impurity density. The transport loss of energy is also influenced by these parameters as well as by the radial electric field structure. The dynamical model of temperature collapse at the density limit consists of the particle balance equation,

$$\frac{d}{dt} n = -\frac{1}{\tau_p} n + S_p \quad (38)$$

the equation of the momentum or the radial electric field

$$\frac{d}{dt} E_r = -\frac{1}{\tau_\phi} E_r - \tilde{J}_r \quad (39)$$

equation for temperature

$$\frac{d}{dt} T = -\frac{1}{\tau_E} T - \frac{P_{rad}}{3 n V} + \frac{P_{abs}}{3 n V} \quad (40)$$

(where convective energy loss is included in  $1/\tau_E$ ), and the particle balance equation for impurity,

$$\frac{d}{dt} n_i = -\frac{1}{\tau_i} n_i + S_i \quad (41)$$

Source terms are shown by  $S_p$ ,  $\tilde{J}_r$ ,  $P_{abs}$  and  $S_i$ , and loss times are expressed as  $\tau_p$ ,  $\tau_\phi$ ,  $\tau_E$ , and  $\tau_i$ .

In plasmas which are confined in toroidal helical plasmas, source terms as well

as loss times are dependent on the plasma parameters as well as on the electric field. Nonlinear dependencies in these terms have been shown to cause self-sustained oscillations [19]. For instance, the dependence of  $\tau_p$  (or  $\tau_E$ ) on the electric field and nonlinearity in  $\tilde{J}_r$  causes the limit cycle oscillation [20], which is attributed to the dithering ELMs [21]. This coupling has also been discussed [22] to understand the electric pulsation which was found in CHS device [23]. The influence of the radial electric field on  $P_{abs}$  [24], together with the dependence of electric field on temperature induces a thermo-electric oscillation [25]. Coupling between the transport coefficient and plasma profiles drives the nonlinear oscillation of confinement time [26]. The influence of temperature on the source of impurities was pointed out to cause oscillations being coupled with the nonlinearity in  $P_{rad}$  [27].

### 3.2 Reduction of Variables

Thus numerous types of self-generated oscillations in the system of dynamical equations are possible. A complete description of possible self-generated oscillations is not in the scope of this article. However, we intend to elucidate a new type of oscillation, by using a simplified dynamical model based on the method of reduction of variables. In the density limit oscillation of the W7-AS experiment [8], it was reported that (i) the relative ratio  $n_i/n_e$  changes little compared to the large amplitude oscillations of temperature or radiation loss and that (ii) hysteresis of loss in the energy transport, if it exists, is much smaller than that in the radiation loss. Based

on these observations, we employ the assumptions, as a first step of the analysis, that (i)  $n_i/n_e$  is constant in time and that (ii)  $\tau_E$  is a single valued function (i.e., no hysteresis in it). Instead of solving Eq.(41), simplification (i) is applied. The next reduction of variable is the electric field. The radial electric field is self-sustained in helical plasmas due to the temperature gradient [28], and is subject to bifurcation, in principle, at a critical temperature [18, 28, 29]. Even though there is a possibility of a bifurcation in transport due to the bifurcation of radial electric field, in this article we do not consider such a mechanism and do not solve the dynamics of radial electric field Eq.(39). The inclusion of the radial electric field bifurcation is left for future work.

Based on these simplifying assumptions, we solve the coupled system of Eqs.(38) and (40). The sudden loss of density, which results from the radiation instability, is predicted to occur. When the radiation instability collapse continues and the temperature becomes lower than the critical value, the symmetry-breaking perturbations of temperature and potential on the magnetic surface become unstable. By the growth of these perturbations, the rapid loss takes place. The details are discussed in the Appendix. The critical condition for this instability is given in terms of the density and temperature as :

$$Tn^{-1} \leq \zeta \equiv \left( \frac{q^2 R^2}{3\chi_0} \frac{n_i}{n_e} \xi \right)^{1/(\gamma+3.5)}, \quad (42)$$

$$y = \frac{2}{\gamma+3.5}$$

When this instability occurs, the rapid plasma loss happens as

$$\frac{d}{dt} n = -\frac{1}{\tau_M} n \quad (43)$$

where the right hand side represents the loss induced by this instability. An estimate of the loss rate of plasma density can be made as (see Appendix for the derivation)

$$\frac{1}{\tau_M} \sim \frac{s+\gamma}{C_a \tau_{rad}} \left( 1 - \left( \frac{Tn^{-1}}{\zeta} \right)^{\gamma+3.5} \right) \quad (44)$$

where  $s$  denotes the response of density to the inhomogeneous temperature perturbation, the coefficient  $k_{\perp}^2 a^2 \sim C_a$  which is of the order unity, and

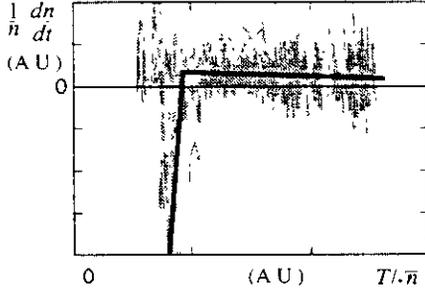
$$\frac{1}{\tau_{rad}} \equiv \frac{1}{3} \left( \frac{n_i}{n_e} \right) \xi n T_0^{-\gamma-1} \quad (45)$$

A minimal model, which is relevant to the study of density limit oscillation dynamics in W7-AS, is constructed from Eqs.(40), (43) and (44).

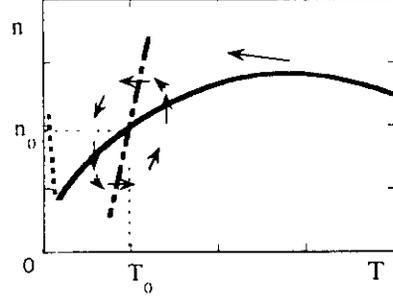
The prediction from Eqs.(43) and (44) is compared with the measurements. (See Fig.6.) It is observed that the rate of density change,  $n^{-1} dn/dt$ , is fitted to a single valued function during the oscillation of energy in W7-AS. The loss rate  $n^{-1} dn/dt$  changes its sign dramatically when the temperature-to-density ratio becomes lower than some critical value.

### 3.3 Model of density limit oscillation

A minimal model for the density limit oscillation is constructed by Eq.(40) together with Eq.(43) and (44). The flow



**Fig.6** Observation on W7-AS stellarator. During the several cycles of density limit oscillation, the rate of density change is correlated with the temperature. Rate of density change,  $n^{-1}dn/dt$ , is fitted to a single valued function of  $T/\bar{n}$  during the limit cycle oscillation. Strong loss of density sets in if temperature becomes very low. Thick solid line is an eye guide. (Units are arbitrary)



**Fig.7** Flow diagram. Solid lines and thick dot-dashed lines represent the stationary solution of Eqs.(43) and (44), respectively. The arrow shows the temporal change in  $n$  and  $T$ ,  $(dT/dt, dn/dt)$ .

diagram is shown schematically on Fig.7.

The stationary solution of Eq.(40) is shown by the solid line, and that for Eq.(43),  $1/\tau_M = 0$ , is plotted by the thick dot-dashed line. Their intersection represents the fixed point  $(T_0, n_0)$ . The temporal change in  $n$  and  $T$ ,  $(dT/dt, dn/dt)$ , is shown by the arrow for various points on the  $(T, n)$  plane. Noting the change of signs near by the fixed point, the flow pattern is found to encircle the fixed point, in the vicinity of the fixed point.

We study the dynamic of variables near the fixed point  $(T_0, n_0)$ , where  $(T_0, n_0)$  satisfy both of the stationary equations, i.e., the limit of  $d/dt \rightarrow 0$  of (40) and (43);

$$\left( \frac{P_{abs}}{3 n_0 V} - \frac{1}{\tau_E(T_0, n_0)} T_0 \right) - \frac{P_{rad}(T_0, n_0)}{3 n_0 V} = 0 \quad (46)$$

and

$$T_0 n_0^{-\gamma} = \zeta \quad (47)$$

The case of strong radiation,  $P_{rad} \gg W/\tau_E$  at  $(T_0, n_0)$ , is considered. Combining Eq (5)

with Eq.(40), one has

$$\frac{d}{dt} T = \frac{P_{abs}}{3 n V} - \frac{1}{3} \left( \frac{n_I}{n} \right) \xi T^{-\gamma} n \quad (48)$$

Noting that  $(T_0, n_0)$  satisfy the equation of stationary state,  $\frac{P_{abs}}{n_0 V} - \left( \frac{n_I}{n} \right) \xi T_0^{-\gamma} n_0 = 0$ ,

Eq.(48) is rewritten as

$$\frac{d}{dt} T = \frac{P_{abs}}{3 n_0 V} \left( \frac{n_0}{n} - 1 \right) + \frac{1}{3} \left( \frac{n_I}{n} \right) \xi \left( T_0^{-\gamma} n_0 - T^{-\gamma} n \right). \quad (49)$$

By using the time rate of change  $\tau_{rad}$  defined

in Eq.(45), Eq.(49) can be rewritten as

$$\frac{d}{dt} \frac{T}{T_0} = \frac{1}{\tau_{rad}} \left( \frac{n_0}{n} - \left( \frac{T_0}{T} \right)^{\gamma} \frac{n}{n_0} \right) \quad (50)$$

The stability of the trajectory near the fixed point is investigated. We put

$$T = T_0(1 + \delta T) \quad (51-1)$$

and

$$n = n_0(1 + \delta n) . \quad (51-2)$$

In the vicinity of  $(T_0, n_0)$ , the Taylor expansions of Eqs.(43), (44) and (50) are made. By use of this expansion, Eq.(43) with Eq.(44) and Eq.(50) are rewritten as, respectively,

$$\frac{d}{dt} \delta n = -\frac{y}{\tau} \delta n + \frac{1}{\tau} \delta T \quad (52)$$

and

$$\frac{d}{dt} \delta T = -\frac{1}{\tau_1} \delta n + \frac{1}{\tau_2} \delta T . \quad (53)$$

where the time constants  $\tau$ ,  $\tau_1$  and  $\tau_2$  are expressed as

$$\frac{1}{\tau} = \frac{(s + \gamma)(\gamma + 3.5)}{C_a} \frac{1}{\tau_{rad}} \quad (54-1)$$

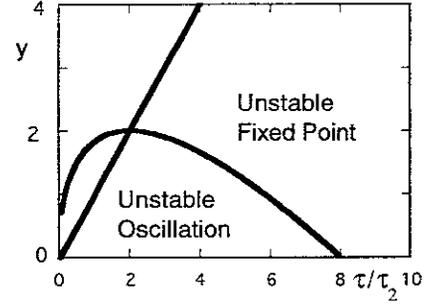
$$\frac{1}{\tau_1} = \frac{2}{\tau_{rad}} , \quad (54-2)$$

$$\frac{1}{\tau_2} = \frac{\gamma}{\tau_{rad}} . \quad (54-3)$$

Equations (52) and (53) are solved assuming that the temporal dependence is written as

$$(\delta n, \delta T) \propto e^{\lambda t} \quad (55)$$

The eigenvalue  $\lambda$  is obtained as



**Fig.8** Parameter region that allows an unstable oscillatory solution. Case of  $\tau_2/\tau_1 = 2$  is shown.

$$\lambda = \frac{\frac{1}{\tau_2} - \frac{y}{\tau} \pm \sqrt{\left(\frac{1}{\tau_2} + \frac{y}{\tau}\right)^2 - \frac{4}{\tau_1 \tau}}}{2} . \quad (56)$$

An oscillatory solution exists if the condition

$$\frac{4}{\tau_1 \tau} > \left(\frac{1}{\tau_2} + \frac{y}{\tau}\right)^2 \quad (57)$$

holds. An unstable oscillation exists if

$$\frac{1}{\tau_2} > \frac{y}{\tau} \quad (58)$$

is satisfied together with Eq.(57).

The limit cycle oscillation is possible in the region that is denoted as 'unstable oscillation' in Fig.8. This diagram presents the condition for the density limit oscillation. A small value of  $\tau/\tau_2$  is necessary. This means that the abrupt reduction of density at  $T n^{-y} \sim \zeta$  is the key for the oscillation. Conditions Eqs.(57) and (58) for unstable oscillation are rewritten, in terms of the

parameter  $\gamma$  that characterizes the radiation rate, as

$$\frac{8(s+\gamma)(\gamma+3.5)}{C_a} > \left( \gamma + \frac{2(s+\gamma)}{C_a} \right)^2 \quad (57')$$

$$\gamma > \frac{2(s+\gamma)}{C_a} \quad (58')$$

In order to satisfy the instability condition, Eq (58'),  $C_a > 2$  is the necessary condition. If it is satisfied, Eqs.(57') and (58') is rewritten as

$$\begin{aligned} \frac{2s}{C_a-2} < \gamma < \\ & \frac{2C_a(7+s)-4s}{(C_a-2)^2} \\ & + \frac{2\sqrt{(C_a(7+s)-2s)^2 - (C_a-2)^2(s^2-7sC_a)}}{(C_a-2)^2} \end{aligned} \quad (59)$$

For intermediate values of  $\gamma$  that satisfy Eq.(59), an unstable oscillation near the fixed point is predicted. The actual range of  $\gamma$  for the limit cycle solution depends on the parameters  $(s, C_a)$ , which appears in the response of plasma to the inhomogeneous perturbation of density. Although quantitative values of the parameters  $(s, C_a)$  are determined by a detailed analysis of transport models, it is beyond the scope of this article to carry this out. Only a qualitative conclusion is possible here. The parameter  $\gamma$  depends on the species of the impurity and range of operation temperature [10]. The condition (59) limits the impurity species that can cause oscillation.

If  $\gamma$  is very large, i.e., the radiation cooling curve  $L_z(T)$  is very steep, so as to

exceed the right hand side of Eq (59), then the fixed point is unstable but not oscillatory. In such cases, the trajectory continuously deviates from the fixed point and might approach to the another fixed point. Usually, the other fixed point exists in a much lower branch of the radiation cooling curve (e.g., dotted line in Fig.2). The density limit collapse occurs, without the recovery of high temperature plasma. The rate of density decay dictates whether the oscillation takes place or radiation collapse continues when the density exceeds the critical density.

In the case of small values of  $\gamma$ ,

Eq.(58') is not satisfied, that is, the fixed point  $(T_0, n_0)$  in Fig.7 is a stable fixed point. The stability of this fixed point means that the steady state is realized in the region where the conditions  $d\{L_z(T)\}/dT < 0$  and  $\partial P_{in}/\partial T < 0$  are satisfied. This is a new type of steady state which is originated from the rapid loss of density with the condition given by Eq.(47).

#### 4. Summary and Discussion

The physics of the density limit phenomena in toroidal helical plasmas based on an analytic point model of toroidal plasmas was discussed. The combination of the transport and radiation loss of energy was analyzed. Firstly, the scaling law of the density limit was derived as a static relation. The dependence of the critical density on the heating power, magnetic field, plasma size and safety factor is explained. Next, the dynamical evolution of the plasma energy and radiation loss is discussed. Employing a simple model of density evolution a limit cycle oscillation is predicted, when a sudden reduction of density

occurs due to the symmetry-breaking radiation instability caused by reaching a critically low temperature. The condition that divides the limit cycle oscillation and the complete radiation collapse was derived. This model seems to explain the density limit oscillation that has been observed on W7-AS [8]. Further comparative studies of the "breathing phenomena" in LHD [6,7] and the density limit oscillation in CHS [16] are necessary to determine whether or not this model also applies.

The dependence of the density limit like  $n_c \sim P^{1/2} B^{1/2} V^{-1/3} q^{-1/4}$  is obtained in the range of  $\gamma = -d \ln(L_Z) / d \ln(T) - 2$ . This form is close to what has been reported from empirical studies [2, 8] but the dependence on the plasma size becomes weaker than  $n_c \propto V^{-1/2}$ . Regression analysis on experimental data has been performed until now on the variables  $B$  and  $P/V$ . In future studies, the independent fitting of the critical density to the heating power and plasma volume is necessary. In addition, the limiting density depends on the ratio of impurity density to the electron density. The heating method could have a strong impact on the source of impurities and in turn change the parameter  $\xi n_i/n_e$ . The density limit could therefore depend on the heating method. This point must be clarified in future experiments.

The impact of indices  $(c_1, c_2, c_3, c_4)$  for the future prospects of the achievable fusion triplet value

$$n\tau_E T = \frac{P}{V} \tau_E^2 \quad (60)$$

is discussed assuming that the parameter  $\xi n_i/n_e$  is constant. Substitution of Eq.(27) provides the relation

$$n\tau_E T \propto n^{2(\alpha+\beta)(1+\alpha)} P^{(1-\alpha)(1+\alpha)} B^{2a_2(1+\alpha)} \times L^{(3\alpha-3+2a_3)(1+\alpha)} q^{-2a_4(1+\alpha)} \quad (61)$$

The density is bound by the density limit,  $n \leq n_c$ . The upper bound of  $n$  provides the upper bound of the fusion triplet

$$n\tau_E T \leq (n\tau_E T)_{\max} \quad (62)$$

The parameter dependence of  $(n\tau_E T)_{\max}$  is derived by substituting the dependencies of the density limit Eqs.(24-1)-(24-4) into Eq.(61), and one has the scaling relation

$$(n\tau_E T)_{\max} \propto P^{d_1} B^{d_2} L^{d_3} q^{-d_4} \quad (63)$$

with

$$d_1 = \frac{(1+\beta)(2+\gamma)}{2+2\alpha+(1-\beta)\gamma} \quad (64-1)$$

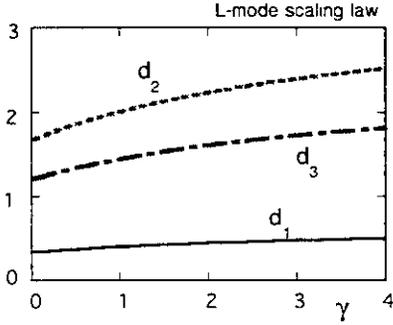
$$d_2 = \frac{2a_2(2+\gamma)}{2+2\alpha+(1-\beta)\gamma} \quad (64-2)$$

$$d_3 = \frac{\{2a_3 - 3(1+\beta)\}(2+\gamma)}{2+2\alpha+(1-\beta)\gamma} \quad (64-3)$$

$$d_4 = \frac{2a_4(2+\gamma)}{2+2\alpha+(1-\beta)\gamma} \quad (64-4)$$

Figure 9 describes the dependencies of indices  $(d_1, d_2, d_3)$  as a function of  $\gamma$ . In the range of  $\gamma = 2$ , the estimate  $(d_1, d_2, d_3, d_4) \approx (0.44, 2.2, 1.6, 1.1)$  is given

for the empirical form of the L-mode confinement law.



**Fig.9** Dependencies of indices  $(d_1, d_2, d_3)$  as a function of  $\gamma$ .

This dependence of fusion triplet describes how the magnetic field, system size and heating power are effective in improving the fusion triplet number. The knowledge of the density limit is essential for the future prospects of helical devices for fusion research. For instance, the predicted critical density is influenced by the difference between the dependence of  $n_c \propto V^{-1/3}$  in this article and  $n_c \propto V^{-1/2}$  in previous empirical fits. (Note that the dependence on volume has not been independently fitted in previous empirical scaling studies.) The weaker dependence of density limit on plasma volume leads to a better extrapolated value. A systematic investigation of experimental data from a number of fusion devices with the presented theoretical ideas as a reference point would be valuable.

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#### Appendix: Density Decay at Low Density

Temperature and potential perturbations can grow due to a radiation instability. The variation of temperature on the magnetic surface is introduced as

$$T(r, \theta) = T_0(r) + \tilde{T}(r, \theta) \quad (\text{A1})$$

The poloidal-angle-dependent component of the energy balance equation is given as

$$\frac{\partial}{\partial t} \tilde{T} = \delta \left\{ -\frac{1}{3} \left( \frac{n_i}{n_e} \right) \xi n T^{-\gamma} + \nabla_{\parallel} \chi_{\parallel} \nabla_{\parallel} T + \nabla_{\perp} \chi_{\perp} \nabla_{\perp} T \right\} \quad (\text{A2})$$

where the symbol  $\delta\{X\}$  implies the poloidally-dependent part of the quantity  $X$ . The inhomogeneity of the heating is neglected, as it is the source of possible variation on a magnetic surface. This is done in order to illustrate the impact of spontaneous symmetry breaking. The relative variation of the radiation rate is parameterized by the coefficient  $s$  as

$$\left( \frac{n_i}{n_e} \right) \xi n = \left[ \left( \frac{n_i}{n_e} \right) \xi n \right]_0 \left( 1 - s \frac{\tilde{T}}{T_0} \right) \quad (\text{A3})$$

A positive value of  $s$  includes the process that the electron density is higher in the region of lower electron temperature. Such a density variation arises from the potential variation. Noting the relation  $\nabla_{\parallel}^2 T = -q^{-2} R^{-2} \tilde{T}$ , Eq.(A3) is rewritten as

$$\frac{d}{dt} \tilde{T} = \gamma_M \tilde{T} \quad (\text{A4})$$

where

$$\gamma_M \equiv \frac{1}{3}(\gamma + s) \left( \frac{n_I}{n_e} \right) \xi n T_0^{-\gamma-1} - \frac{\chi_{\parallel}}{q^2 R^2} \quad (\text{A5})$$

In calculating the growth rate  $\gamma_M$ , the perpendicular diffusion term is neglected, because the perpendicular loss rate is smaller than the radiation loss rate after the radiation collapse takes place. Noticing the dependence of the parallel conductivity on the temperature,

$$\chi_{\parallel} = \chi_0 n^{-1} T^{2.5} \quad (\text{A6})$$

the instability condition  $\gamma_M > 0$  can be rewritten as

$$T n^{-\gamma} \leq \zeta \equiv \left( \frac{q^2 R^2}{3 \chi_0} \frac{n_I}{n_e} \xi \right)^{1/(\gamma+3.5)}, \quad (\text{A7})$$

$$y = \frac{2}{\gamma+3.5}$$

When this instability occurs, the rapid plasma loss occurs. We use a simple model of

$$\frac{d}{dt} n = -\frac{1}{\tau_M} n \quad (\text{A8})$$

where the right hand side represents the loss induced by this instability. An estimate of the loss rate of plasma density can be made, by use of the growth rate  $\gamma_M$  and the perpendicular wave number  $k_{\perp}$  of the instability Eq.(A4), as

$$\frac{1}{\tau_M} \approx \frac{\gamma_M}{k_{\perp}^2 a^2} \quad (\text{A9})$$

With the order estimate of

$$k_{\perp}^2 a^2 \sim C_a$$

which is of the order unity, one obtains

$$\frac{1}{\tau_M} \sim \frac{s + \gamma}{C_a \tau_{rad}} \left( 1 - \left( \frac{T n^{-1}}{\zeta} \right)^{\gamma+3.5} \right) \quad (\text{A10})$$

where

$$\frac{1}{\tau_{rad}} \equiv \frac{1}{3} \left( \frac{n_I}{n_e} \right) \xi n T_0^{-\gamma-1} \quad (\text{A11})$$

Rapid plasma loss is predicted to occur at low temperature, Eq.(A7).

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